

Reliability and Durability of Materials & Components for SOFCs

Edgar Lara-Curzio
Metals & Ceramics Division
Oak Ridge National Laboratory
Oak Ridge, TN 37831-6069

SECA Core Technology Program Review
February 20, 2002

Acknowledgments

Work sponsored by the US Department of Energy, Office of Fossil Energy, SECA Core Technology Program at ORNL under Contract DE-AC05-00OR22725 with UT-Battelle, LLC.

M. Radovic, B. Armstrong, Claudia Walls, Michael Lance
Metals & Ceramics Division
Oak Ridge National Laboratory

Outline

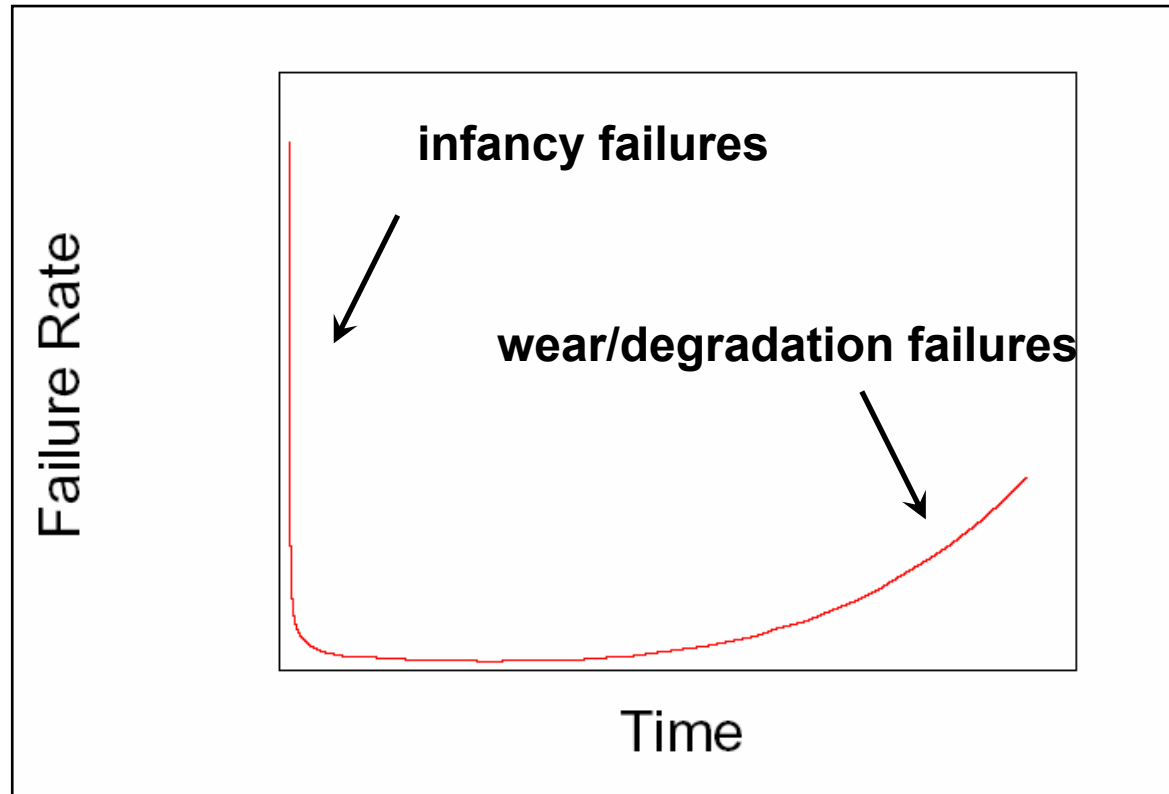
- Objectives
- Predicting Reliability
 - Infancy Failures
 - Wear/Degradation-induced Failure
- Evaluation of Material Properties
- Implications of Results for Manufacturing
- Future Work
 - Phase Identification and Micromechanical Stress Calculations

Objectives

In collaboration with industrial teams and other Core Technology Program participants,

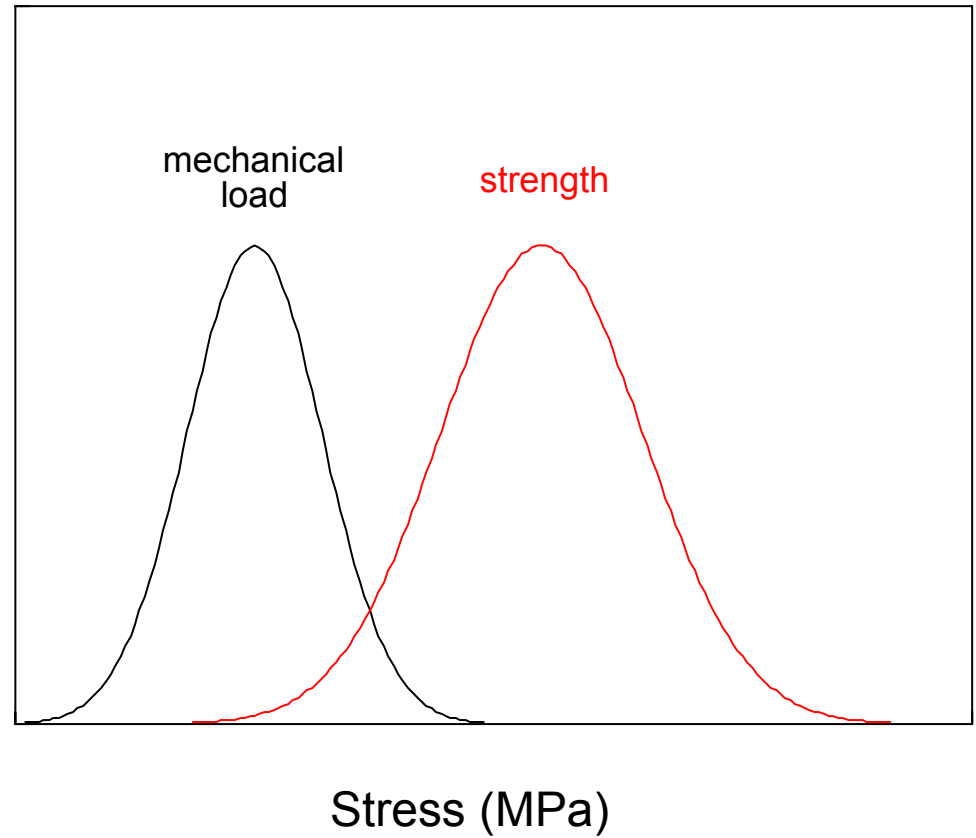
- *To develop/adapt/recommend test techniques to evaluate the properties and behavior of materials and components for SOFC.*
- *To identify and understand the mechanism responsible for the failure of materials and components for SOFCs.*
- *To develop methodologies for predicting the durability and reliability of materials and components for SOFCs.*

A bathtub curve describes the evolution of the failure rate for most complex systems



What information is needed to predict infancy failures of SOFCs?

- Stress distribution
- Distribution of strengths



What information is needed to predict infancy failures of SOFCs?

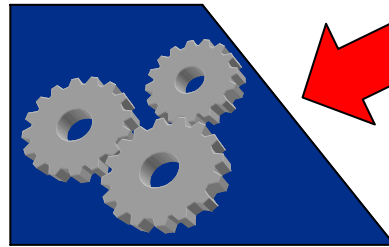
Stress Distribution

- Geometry
- Temperature Distribution
- Mechanical Loads
- Boundary Conditions
- Elastic Constants
- Volumetric Changes
- Thermal Expansion

Elastic Constants as a function of:

- porosity
- temperature

Volumetric Changes due to reduction



Distribution of Strengths

Strength as a function of:

- porosity
- temperature
- size

Toughness

- interfacial

Reliability/Probability of Failure

OAK RIDGE NATIONAL LABORATORY
U. S. DEPARTMENT OF ENERGY



Characterized Materials

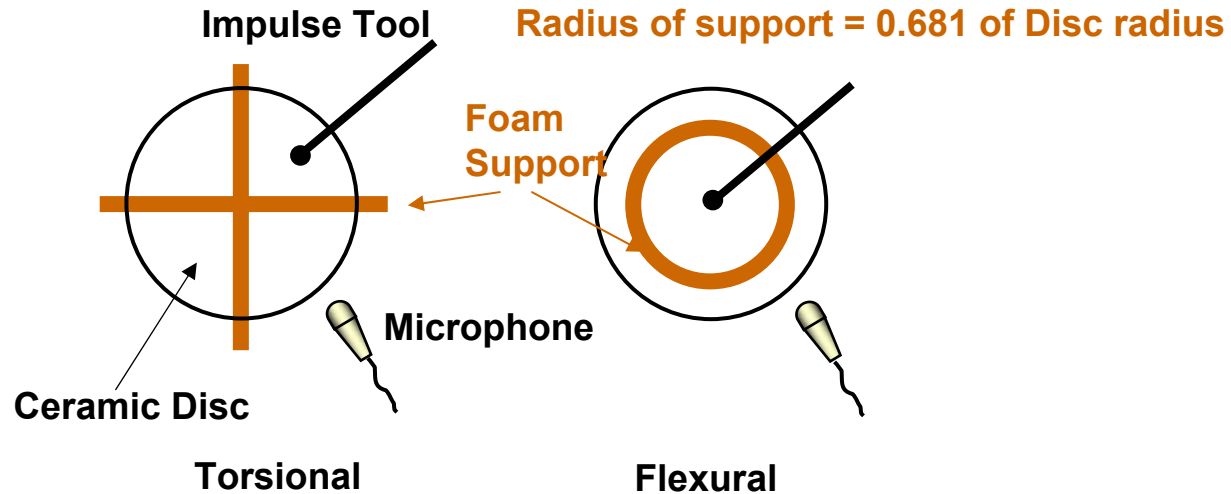
8YSZ - Zirconia stabilized with 8mol% Yttria

NiO/YSZ - 75mol%NiO/25mol%YSZ, a precursor to Ni/YSZ anode

	8YSZ			NiO/YSZ				
# of laminated layers	1	2	4	2	4	6	4	4
Nominal Thickness, mm	0.25	0.50	1.00	0.50	1.00	1.50	1.00	1.00
Pore former, vol%	0	0	0	30	30	30	25	0
Sintering conditions	1400 °C for 2 h			1400 °C for 2 h				
Measured porosity, %	6.2 ±1.0	6.3 ±1.5	5.7 ±1.2	-	22.8 ±1.1	-	19.8 ±0.9	6.8 ±0.3

Young's and Shear Moduli

Impulse Excitation Technique (ASTM C1259-98)



$$E_{t,f} = \frac{[37.699f_{t,f}^2 D^2 m(1 - \mu^2)]}{K_{t,f}^2 h^3}$$

$E_{t,f}$ = Young's modulus as measured by torsional/flexural resonance

m = mass of the disc

t = height of the disc

D = diameter of the disc

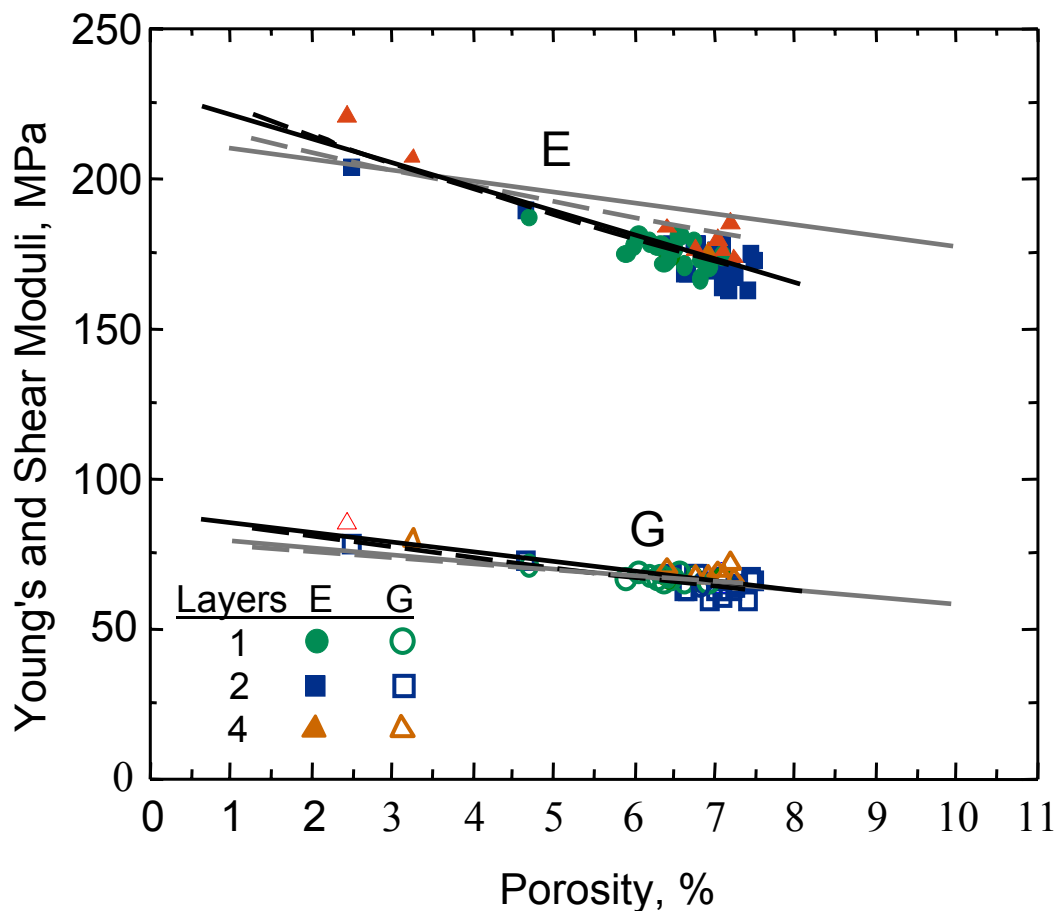
$F_{t,f}$ = fundamental torsional/flexural resonant frequency of the disc

K_t = a correction factor (ASTM C1259-98)

μ = Poisson's ratio

Young's and Shear Moduli

8mol%YSZ as a function of porosity



This work:

$$E = 229.85 (1 - 3.80 p)$$

$$G = 88.24 (1 - 3.69 p)$$

$$E = 234.54 \exp(-4.35 p)$$

$$G = 90.20 \exp(-4.51 p)$$

Literature*:

$$E = 219.53 (1 - 2.50 p)$$

$$G = 83.22 (1 - 2.39 p)$$

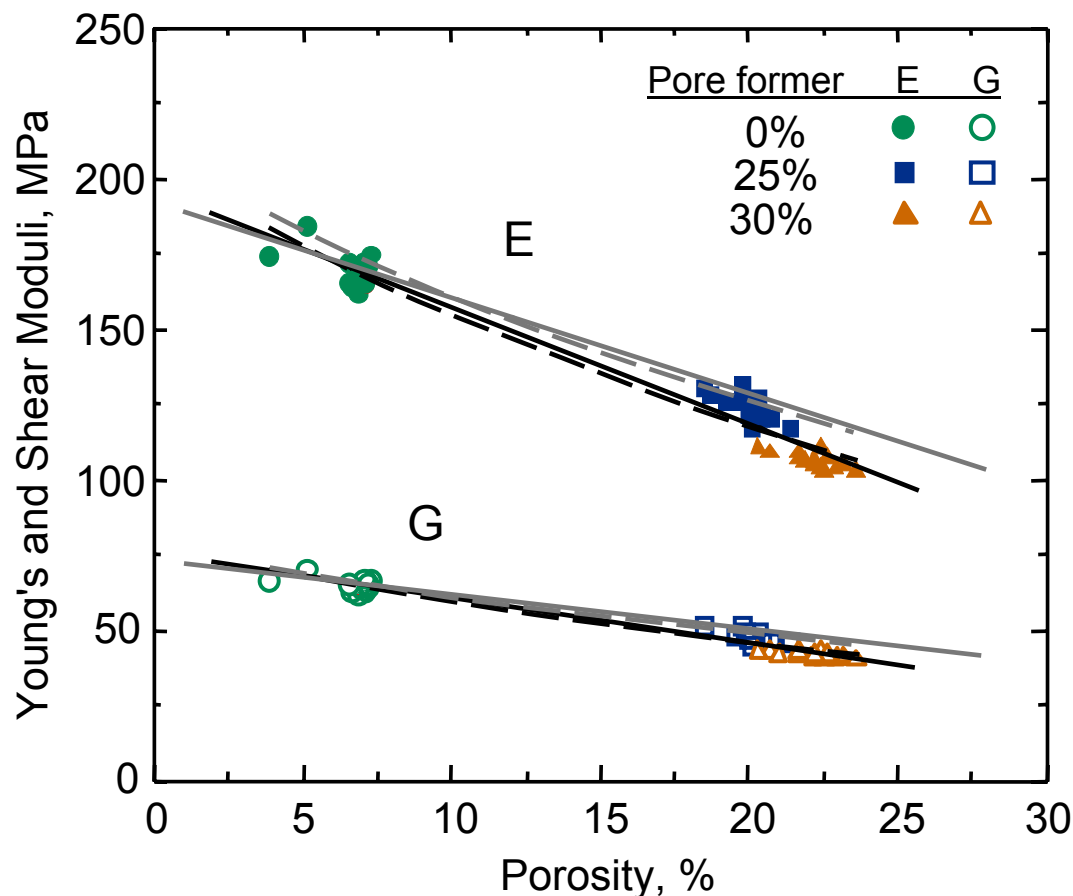
$$E = 220.27 \exp(-2.76 p)$$

$$G = 83.47 \exp(-2.63 p)$$

*A. Selcuk and A. Atkinson, *J. Euro. Ceram. Soc.*, **17** (1007) p.1523

Young's and Shear Moduli

75mol%NiO/YSZ as a function of porosity



This work:

$$E = 195.49 (1 - 1.96 p)$$

$$G = 75.15 (1 - 1.93 p)$$

$$E = 204.47 \exp(-2.76 p)$$

$$G = 78.09 \exp(-2.65 p)$$

Literature*:

$$E = 205.46 (1 - 2.10 p)$$

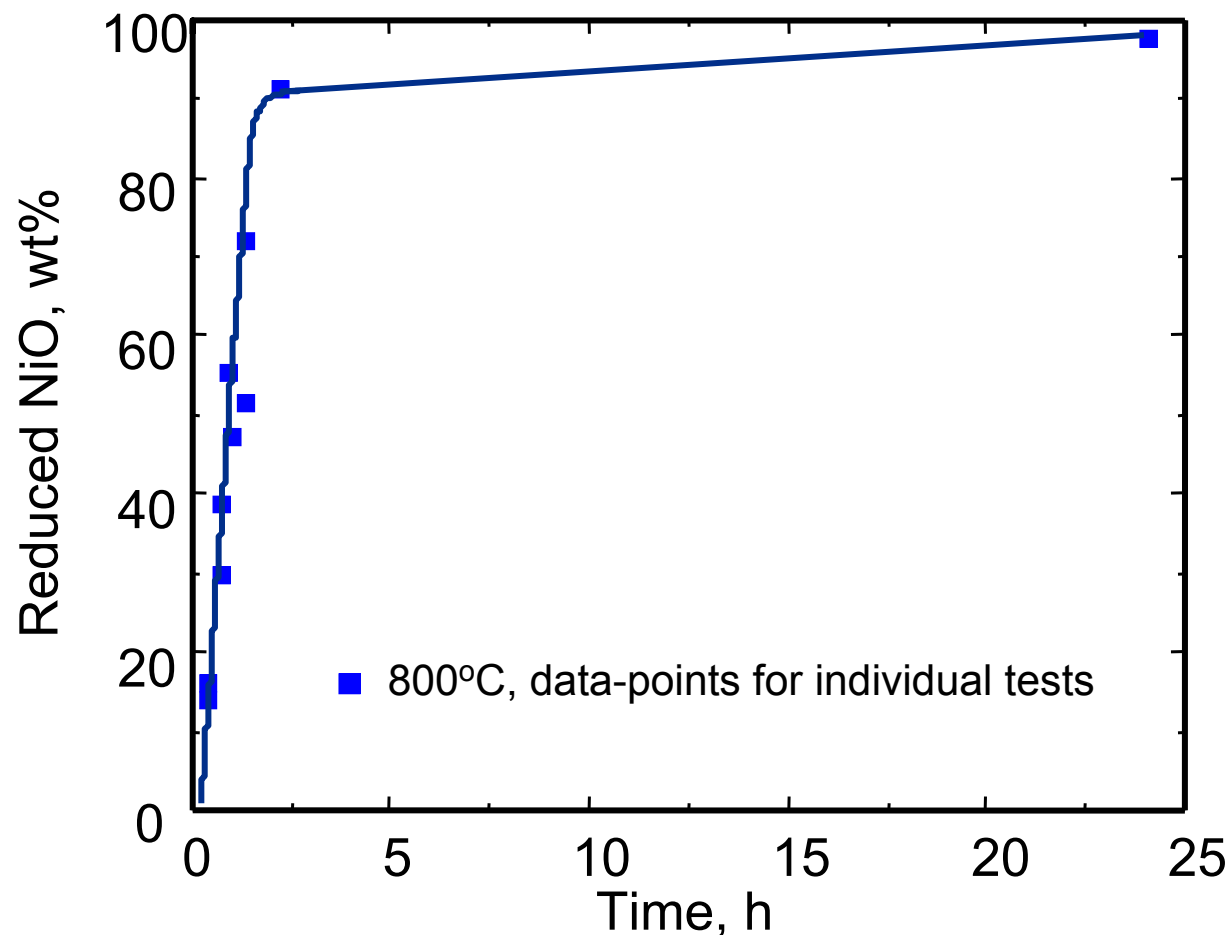
$$G = 77.04 (1 - 2.03 p)$$

$$E = 207.13 \exp(-2.48 p)$$

$$G = 78.04 \exp(-2.38 p)$$

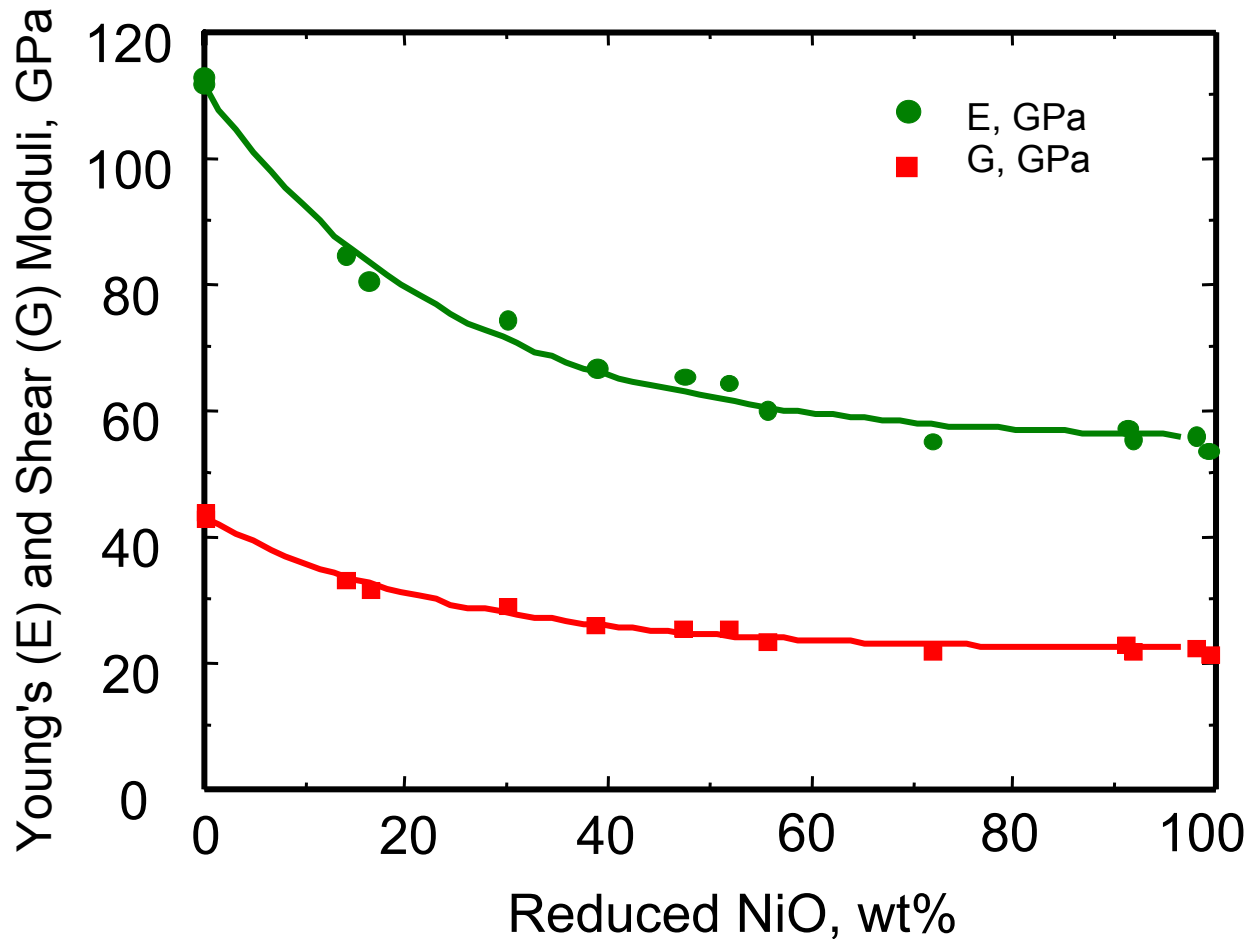
*A. Selcuk and A. Atkinson, *J. Euro. Ceram. Soc.*, **17** (1007) p.1523

Thermogravimetric Analysis (TGA) of NiO/YSZ Reduction



Reduction of NiO measured for different samples. Samples were reduced for a different period of time at 800°C in 4%H₂-96%Ar gas mixture

Young's and Shear Moduli vs. wt% of Reduced NiO in Anode



What information is needed to predict infancy failures of SOFCs?

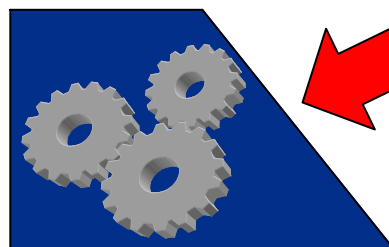
Stress Distribution

- Geometry
- Temperature Distribution
- Mechanical Loads
- Boundary Conditions
- Elastic Constants
- Volumetric Changes
- Thermal Expansion

Elastic Constants as a function of:

- porosity
- temperature

Volumetric Changes due to reduction



Distribution of Strengths

Strength as a function of:

- porosity
- temperature
- size

Toughness

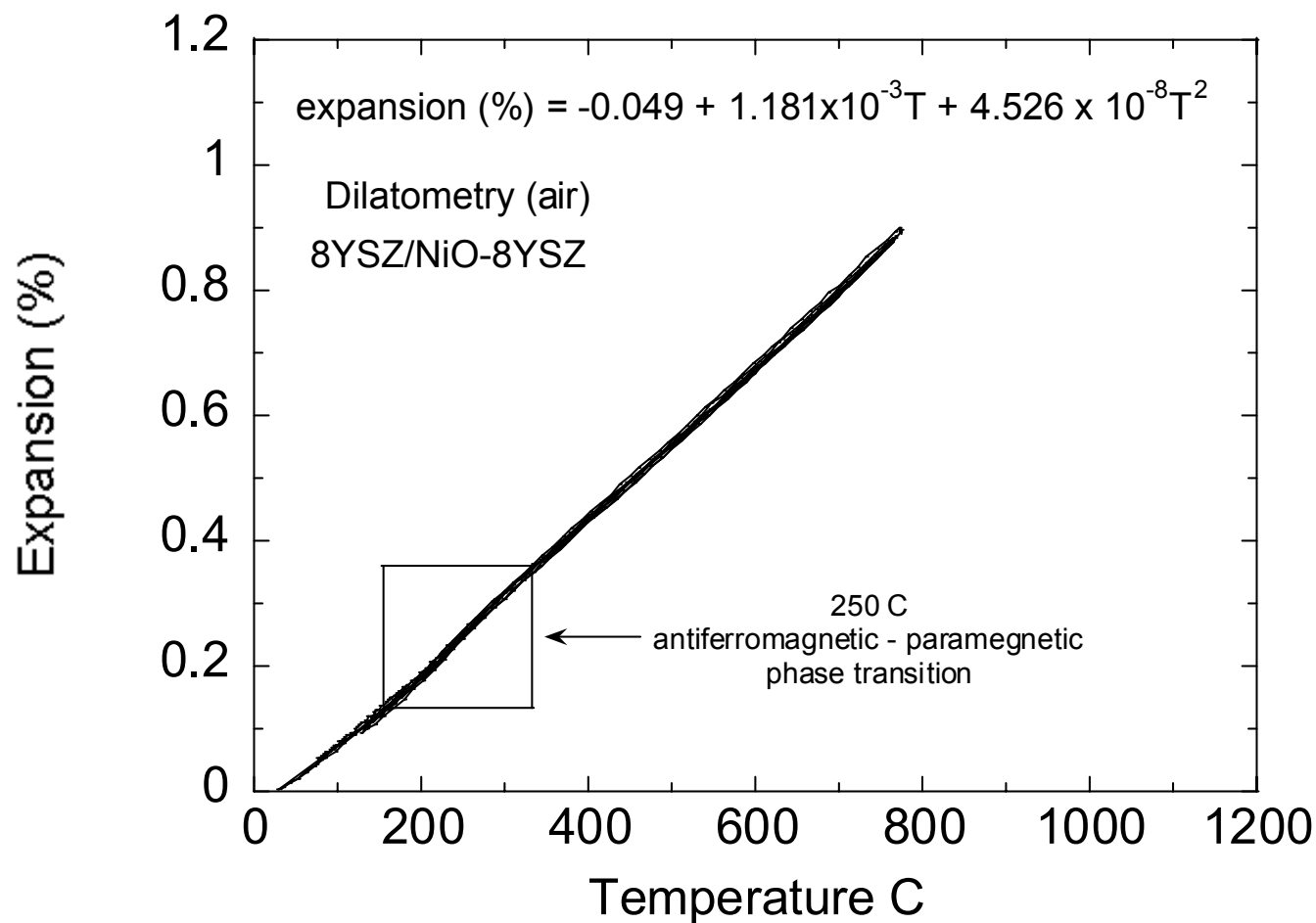
- interfacial

Reliability/Probability of Failure

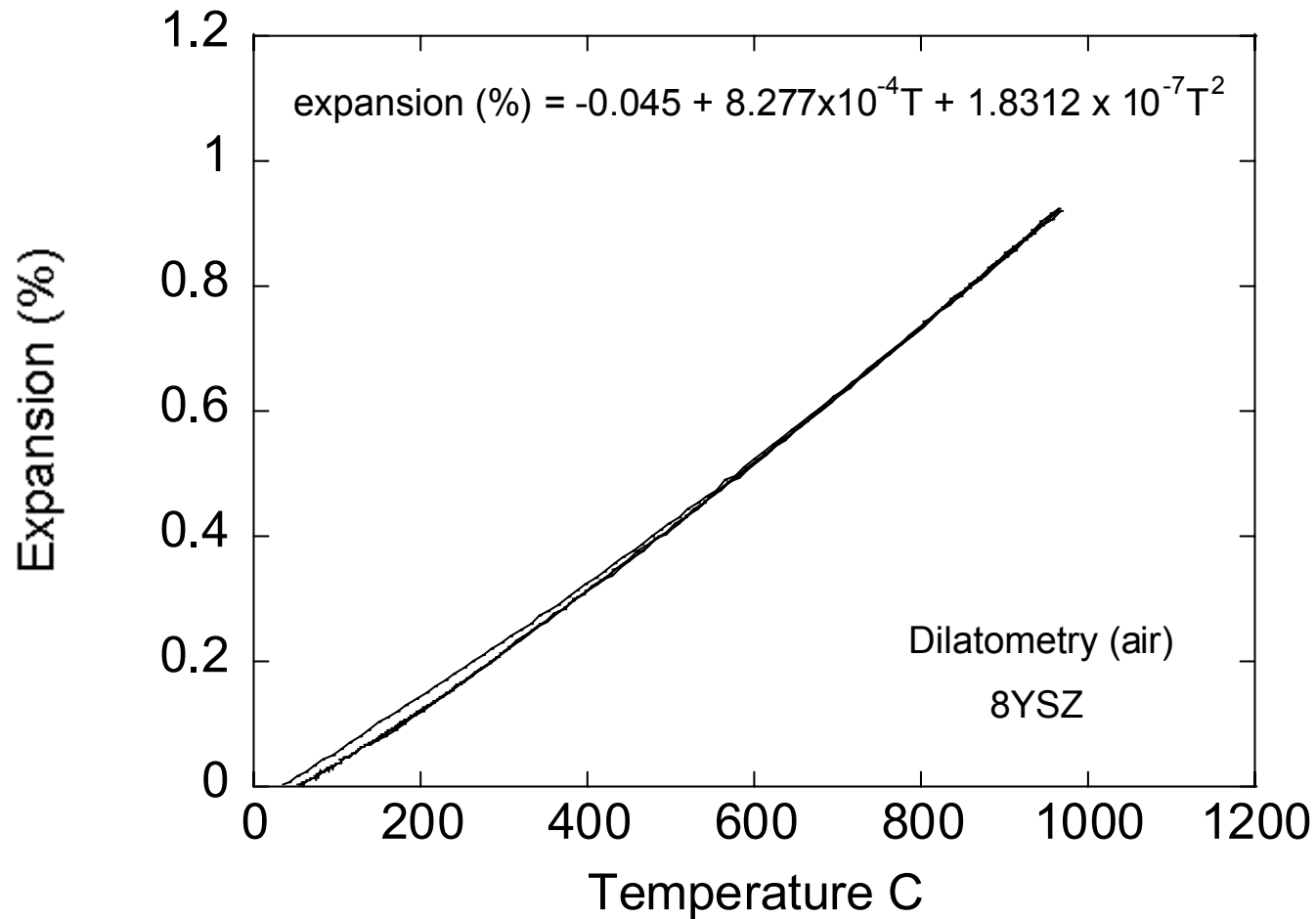
OAK RIDGE NATIONAL LABORATORY
U. S. DEPARTMENT OF ENERGY



Thermal Expansion of NiO/8YSZ



Thermal Expansion of 8YSZ



What information is needed to predict infancy failures of SOFCs?

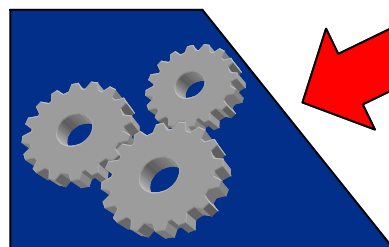
Stress Distribution

- Geometry
- Temperature Distribution
- Mechanical Loads
- Boundary Conditions
- Elastic Constants
- Volumetric Changes
- Thermal Expansion

Elastic Constants as a function of:

- porosity
- temperature

Volumetric Changes due to reduction



Distribution of Strengths

Strength as a function of:

- porosity
- temperature
- size

Toughness

- interfacial

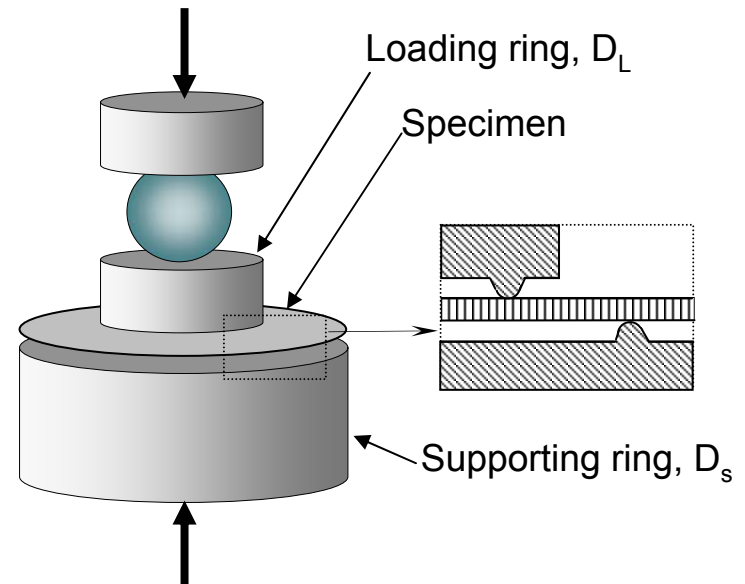
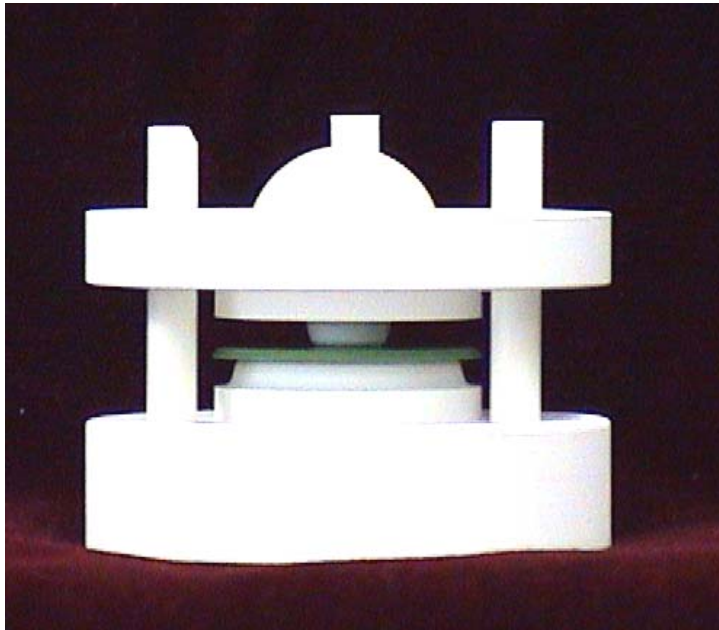
Reliability/Probability of Failure

OAK RIDGE NATIONAL LABORATORY
U. S. DEPARTMENT OF ENERGY



Biaxial Strength

Ring-on-ring Testing (ASTM C1499-01)

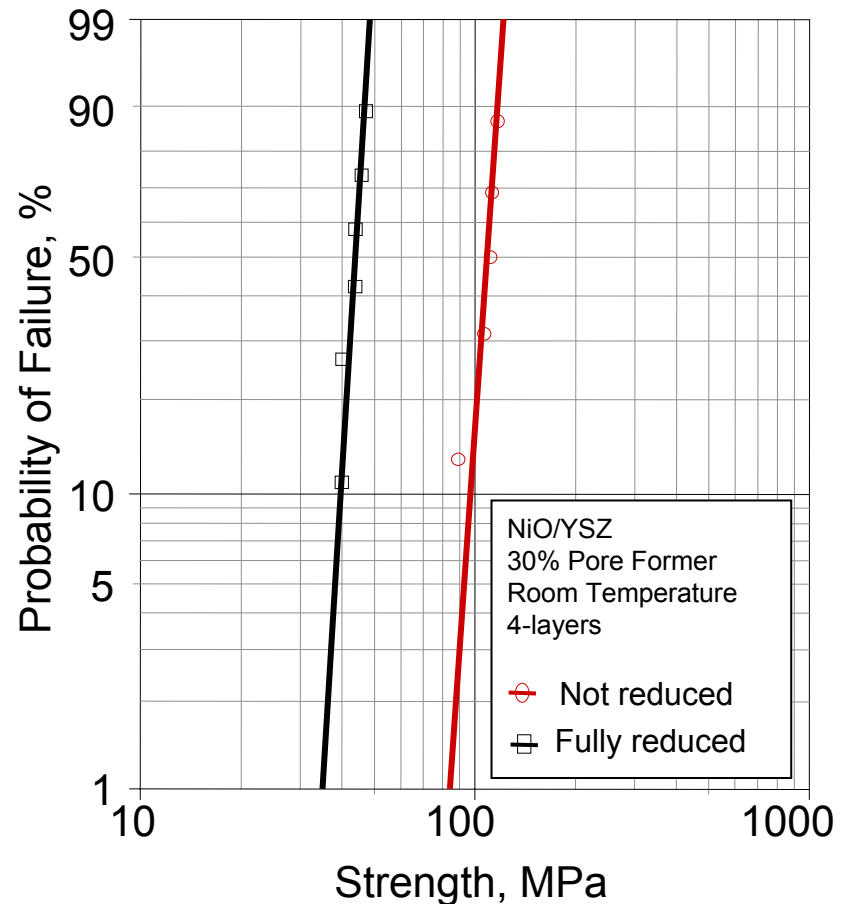
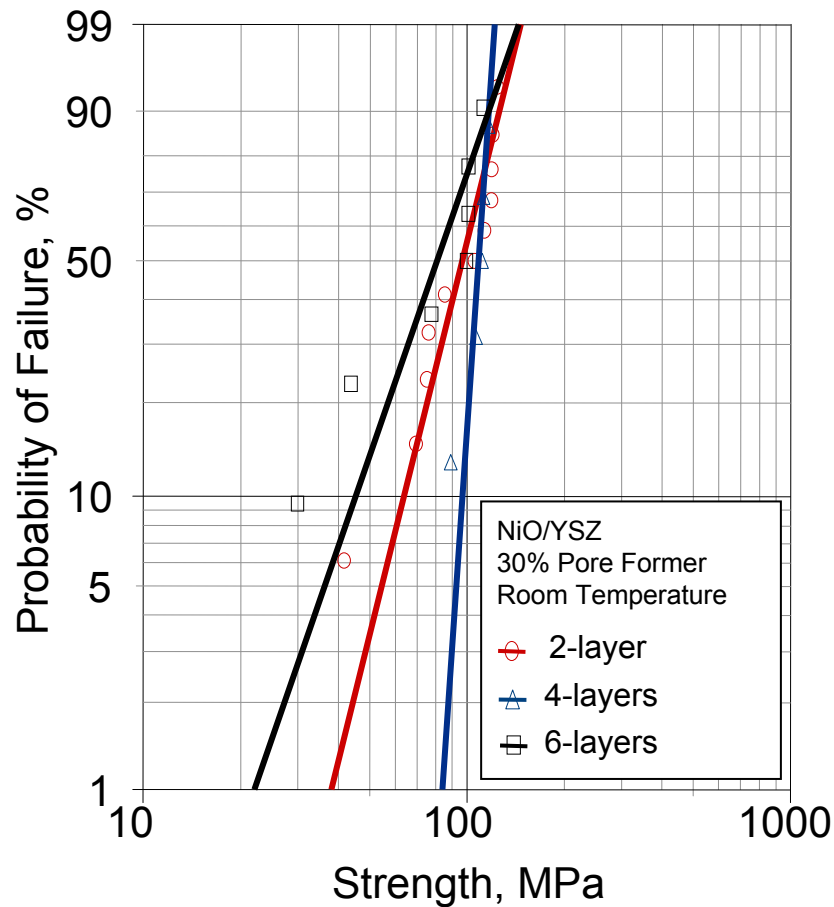


$$\sigma_f = \frac{3F}{2\pi h^2} \left[(1-\nu) \frac{D_s^2 - D_l^2}{2D^2} + (1+\nu) \ln \frac{D_s}{D_l} \right]$$

where F is breaking load, h sample thickness, ν is Poisson's ratio and D , D_s and D_l are diameter of sample, supporting ring and loading ring, respectively

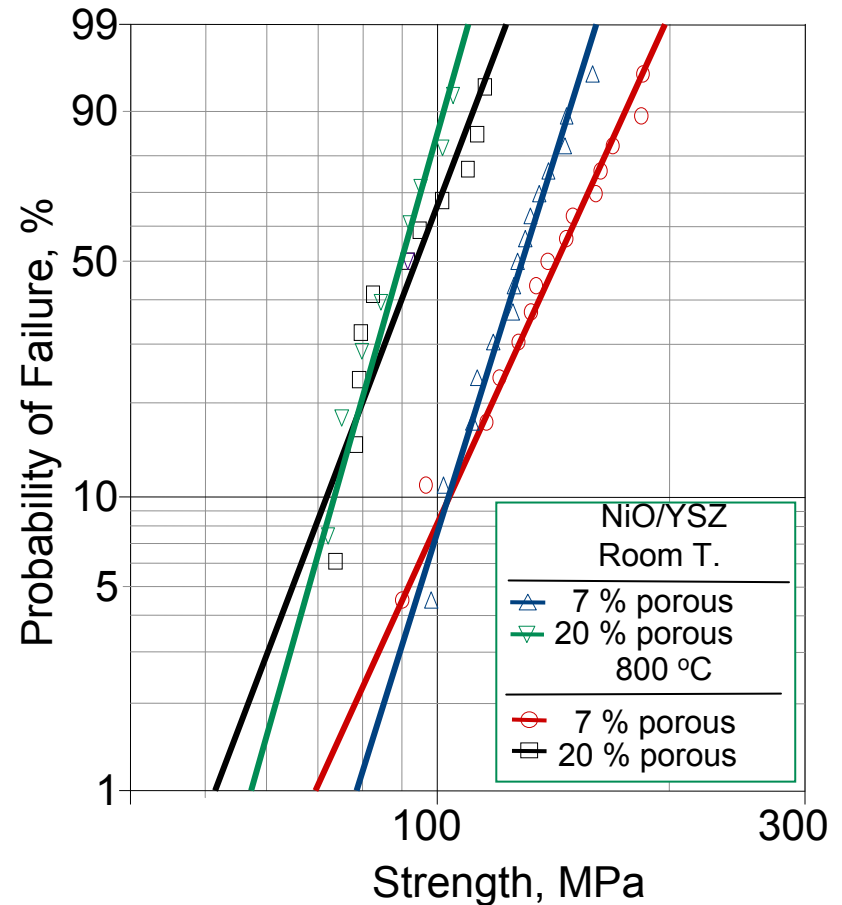
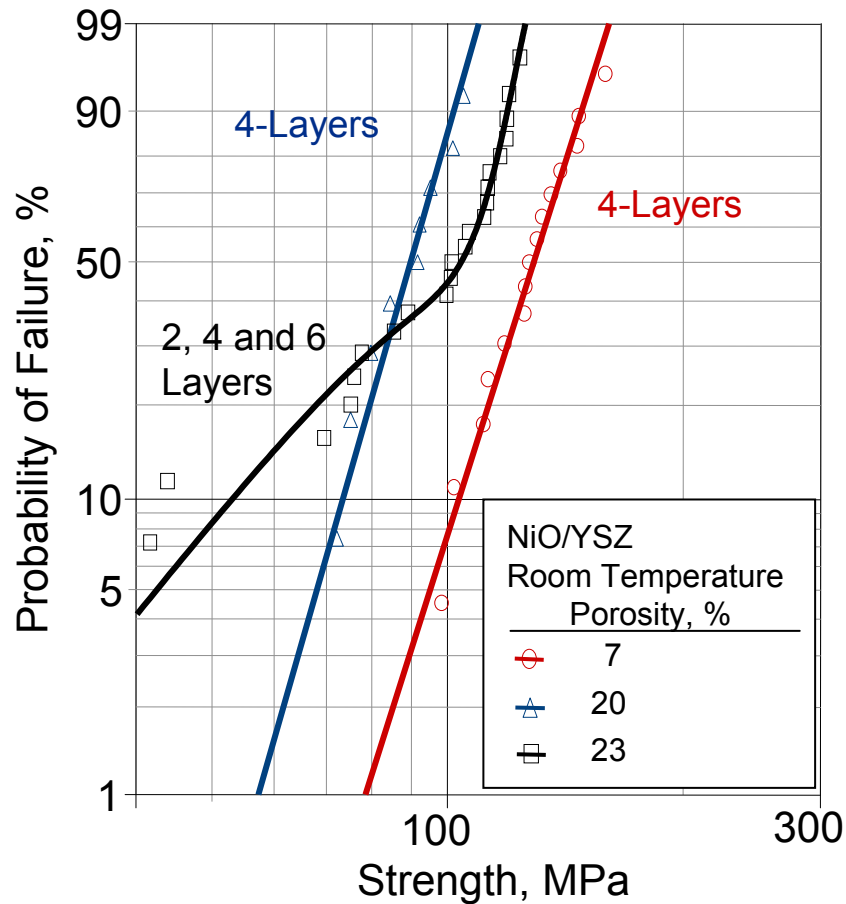
Biaxial Strength

NiO/8YSZ – Weibull plots



Biaxial Strength

NiO/YSZ – Weibull plots



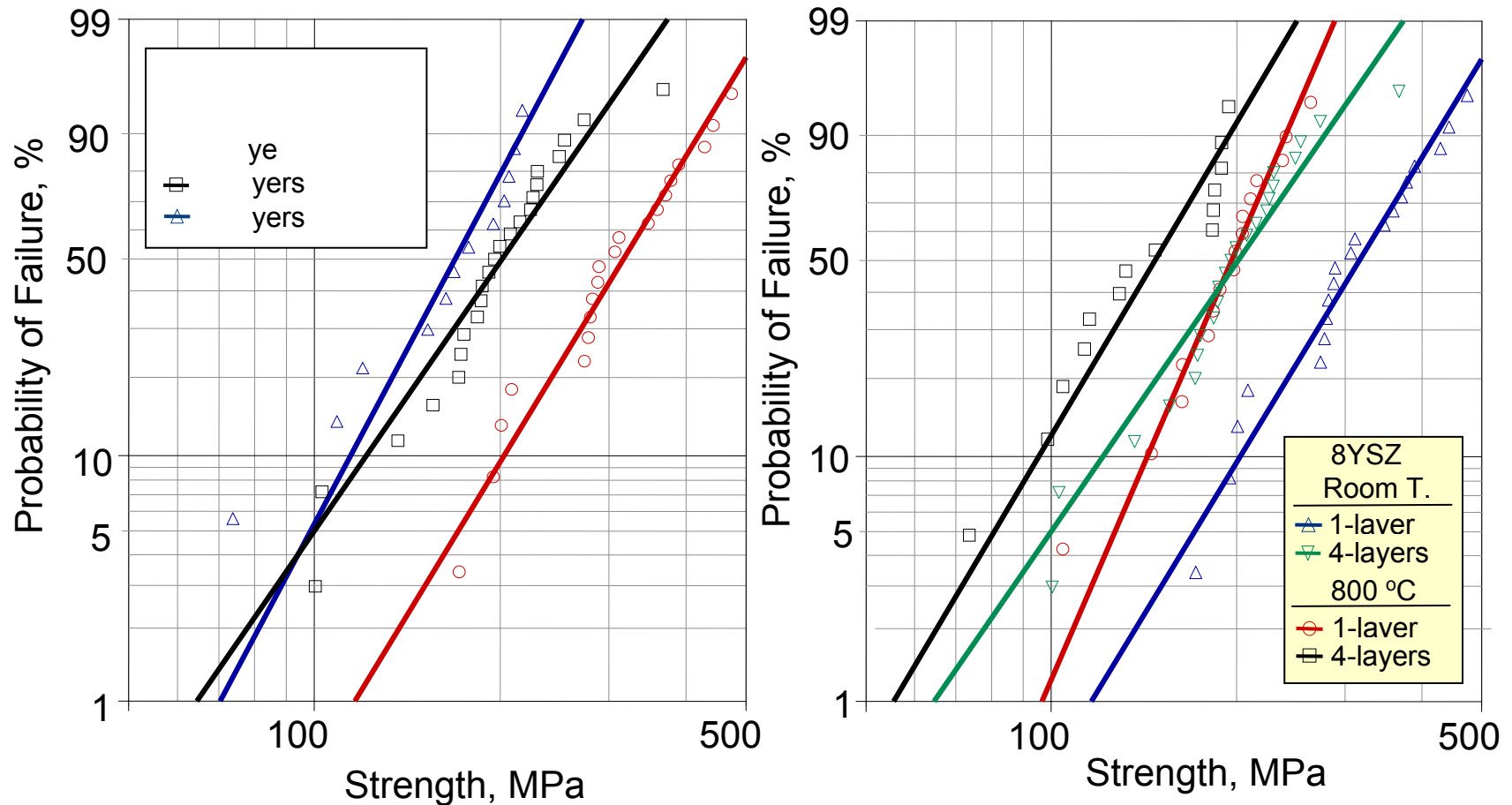
Biaxial Strength

NiO/YSZ – Summary of Weibull statistics

Characteristic strength (MPa) / Weibull modulus Average strength ± Standard Deviation (MPa)			
NiO/YSZ			
# layers -Pore former/Porosity, %	2 - 30/23	4 - 30/23	6 - 30/23
Room Temperature	105.9 / 3.5 95.3 ± 27.2	111.3 / 16.5 107.3 ± 10.8	90.6 / 3.3 80.8 ± 32.1
Ni/YSZ (Fully reduced NiO/YSZ)			
# layers-Pore former/Porosity, %	-	4 - 30/41	-
Room Temperature	-	44.7 / 18.7 43.5 ± 2.9	-
NiO/YSZ			
# layers-Pore former/Porosity, %	4 - 0/7	4 - 25/20	2, 4 and 6 - 30/23
Room Temperature	134.6 / 8.6 127.4 ± 17.3	93.3 / 9.4 88.5 ± 11.4	79.6 / 3.4 - 115.4 / 17.4 65.4 ± 25.3 - 111.6 ± 7.6
800oC	152.3 / 5.8 140.9 ± 28.6	98.9 / 7.0 92.6 ± 15.1	-

Biaxial Strength

8YSZ – Weibull plots



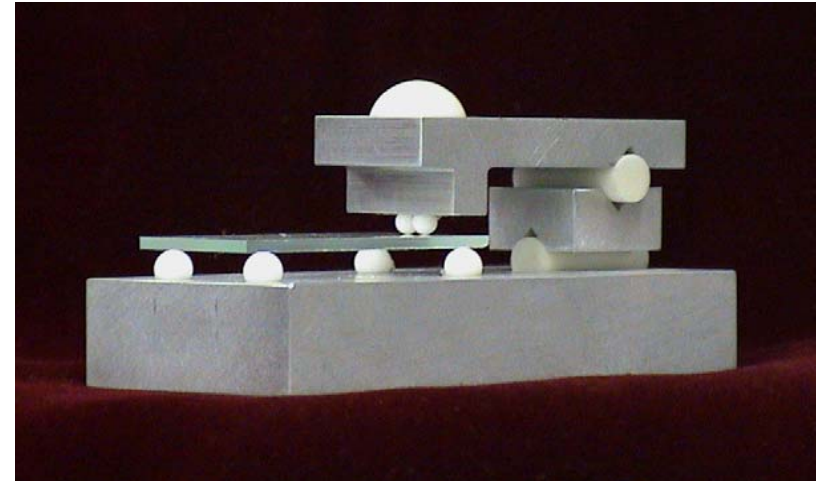
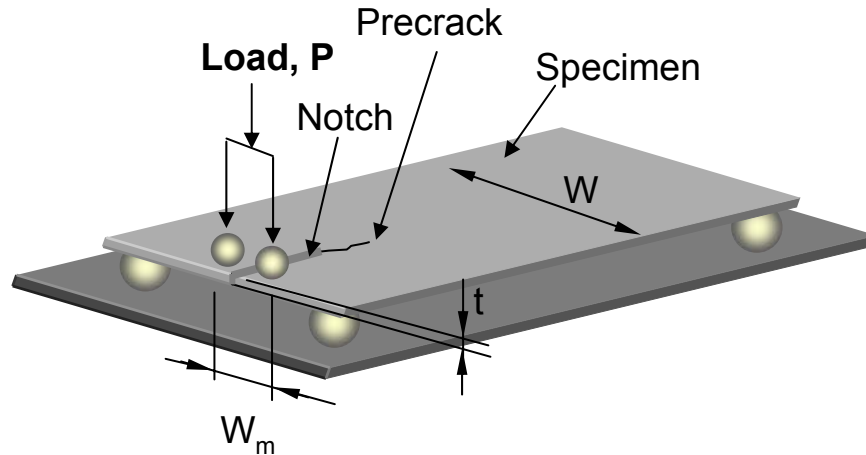
Biaxial Strength

8YSZ – Summary Weibull Statistics

8mol%YSZ		Characteristic strength (MPa) / Weibull modulus Average strength $\pm$ Standard Deviation (MPa)		
Number of layers	1	2	4	
Room Temperature	345.3 / 4.2 313.7 $\pm$ 84.8	182.4 / 4.8 166.4 $\pm$ 45.4	222.2 / 3.7 201.5 $\pm$ 56.5	
600°C	-	-	131.5 / 4.4 127.10 $\pm$ 29.4	
800°C	208.9 / 5.9 193.9 $\pm$ 38.8	175.4 / 8.2 166.2 $\pm$ 25.6	160.5 / 4.3 145.5 $\pm$ 41.1	

Fracture Toughness

Double Torsion Testing



$$K_I = PW_m \left[\frac{3(1+\nu)}{Wt^4\xi} \right]^{1/2}, \xi = 1 - 1.26(t/W) + 2.4(t/W)\exp[-\pi W/(2t)]$$

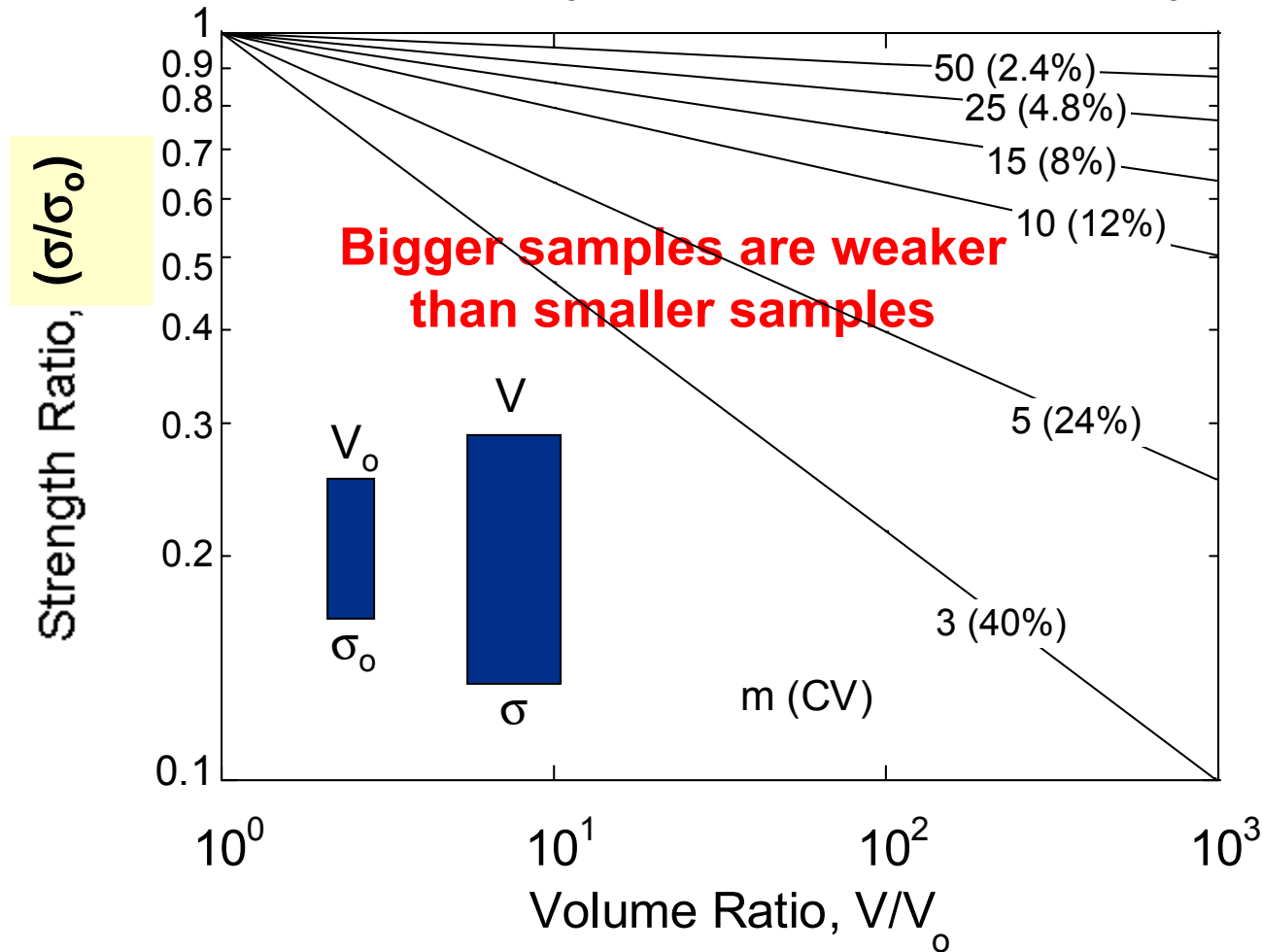
Precracked @ 0.02 mm/min and tested @ 1 mm/min

4 layers	8YSZ	NiO/YSZ
K_{IC} , MPa m ^{1/2}	1.65 ± 0.02	1.04 ± 0.13

Implications of stochastic nature of strength

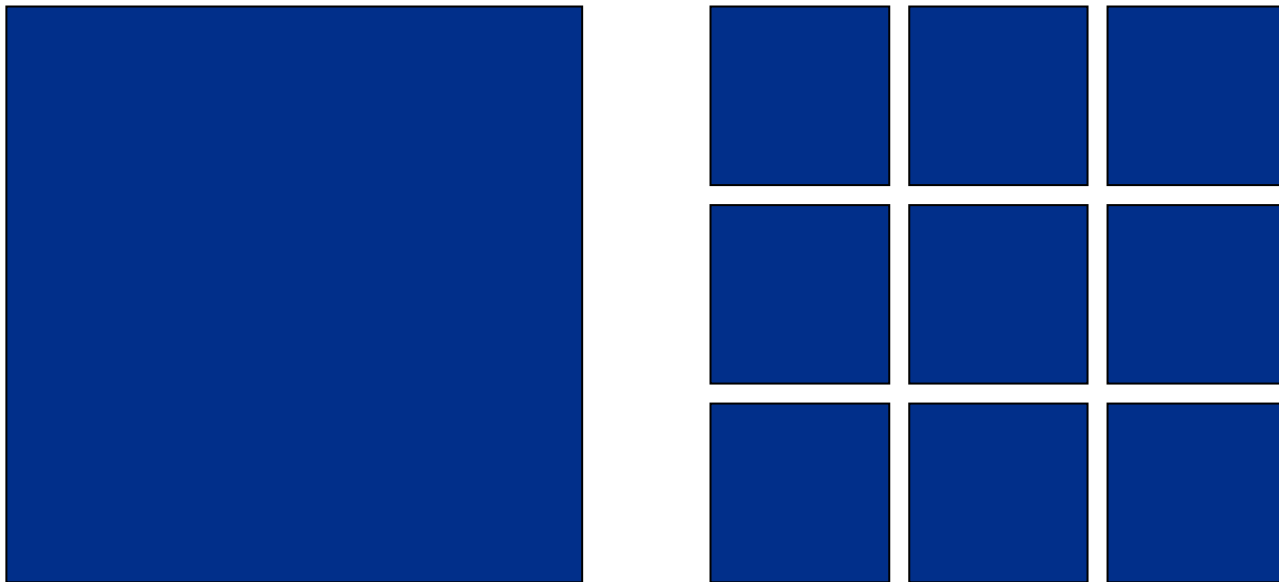
Implications of stochastic nature of strength

If a specimen of size V_o has average strength σ_o , then

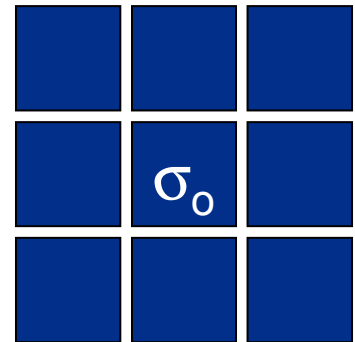
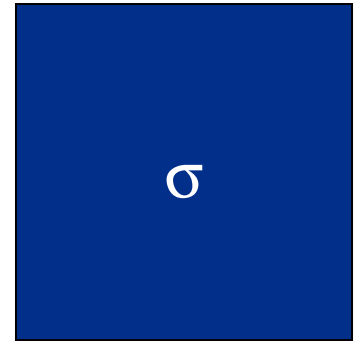
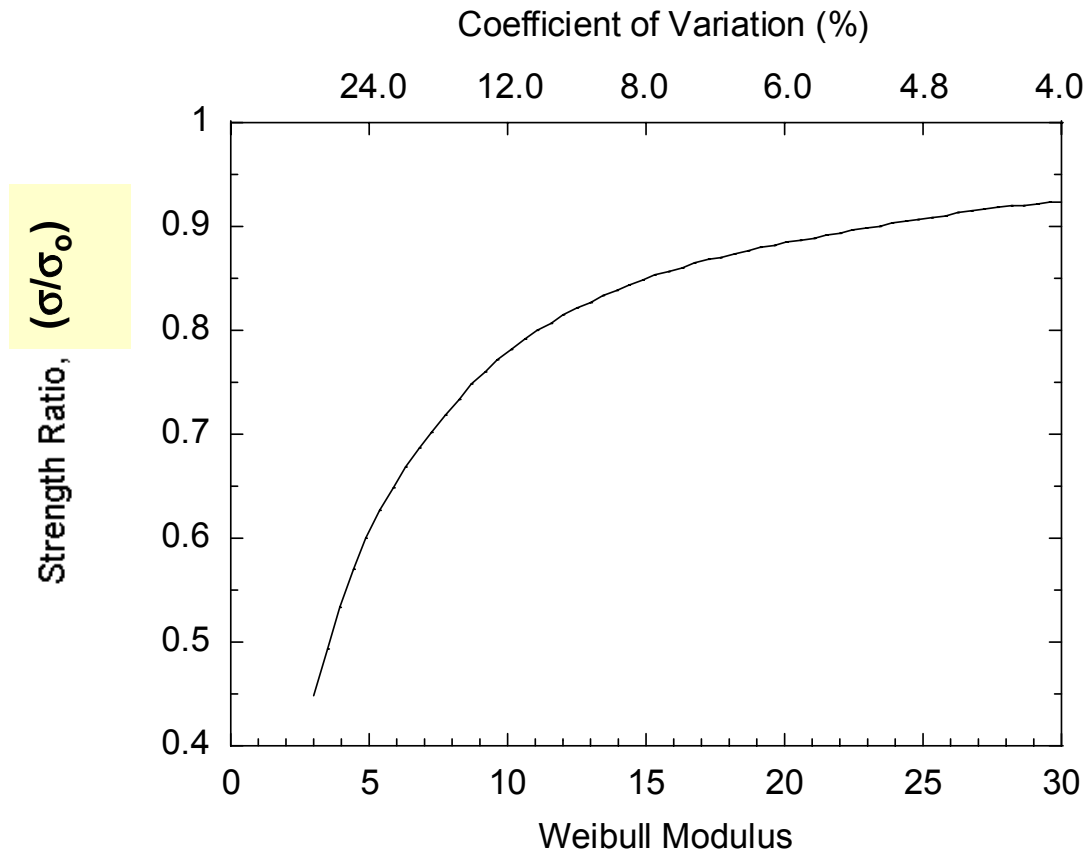


Impact of Stochastic Strength on Manufacturing Decisions

Instead of building large cells, which are weaker than smaller cells, why not using a larger number of smaller cells to cover the same surface area?



Impact of Stochastic Strength on Manufacturing Decisions

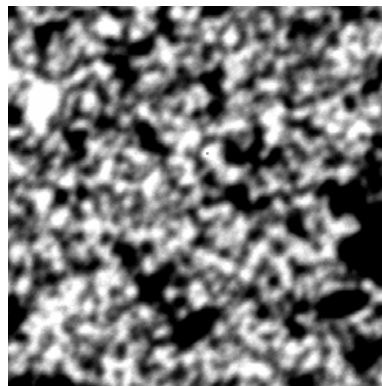
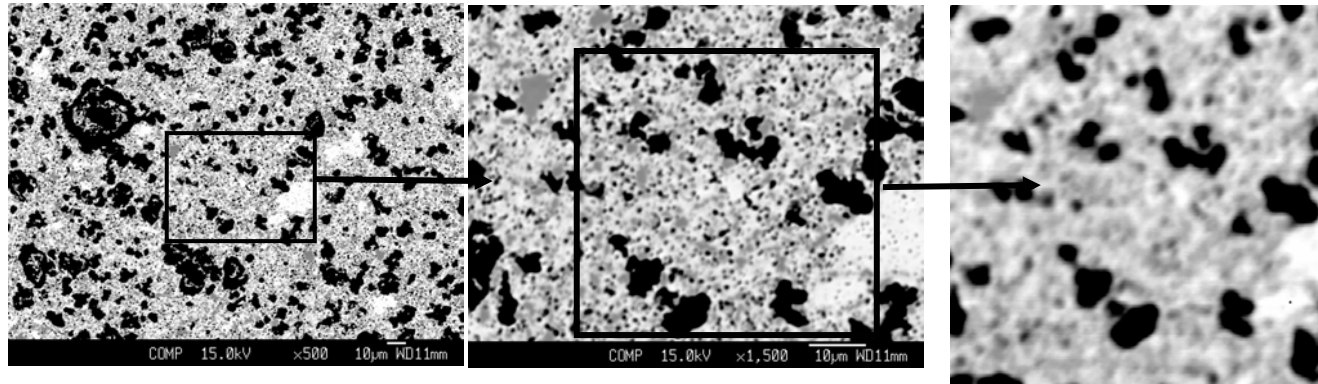


$$V/V_0 = 9$$

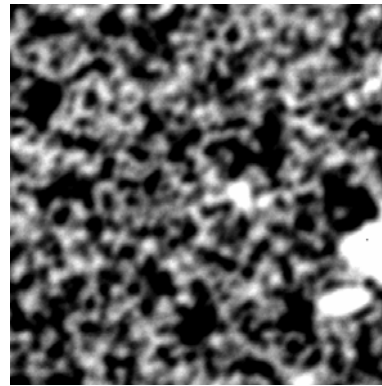
Future Work

- Complete implementation of methodology to predict reliability of model system (geometry, materials).
- Verification of stress predictions using Raman spectroscopy.
- Determination of fracture toughness and adhesion strength of thin coatings.
- Effect of thermal cycling on reliability and durability
- Long-term reliability
- Compositional Analysis and Micromechanical Modeling

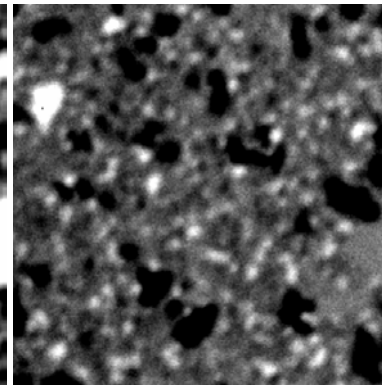
Compositional Analysis and Micromechanical Modeling



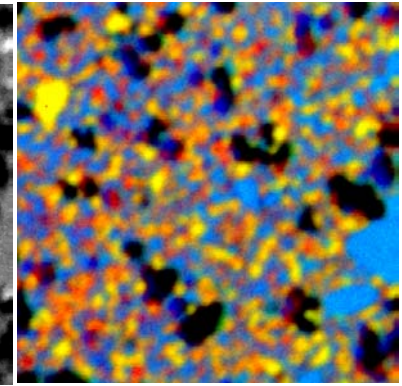
Ni
white – maximum
Black -minimum



Zr
white – maximum
Black -minimum

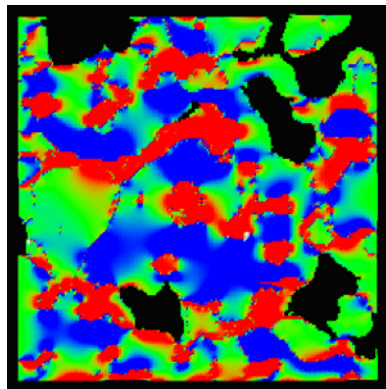
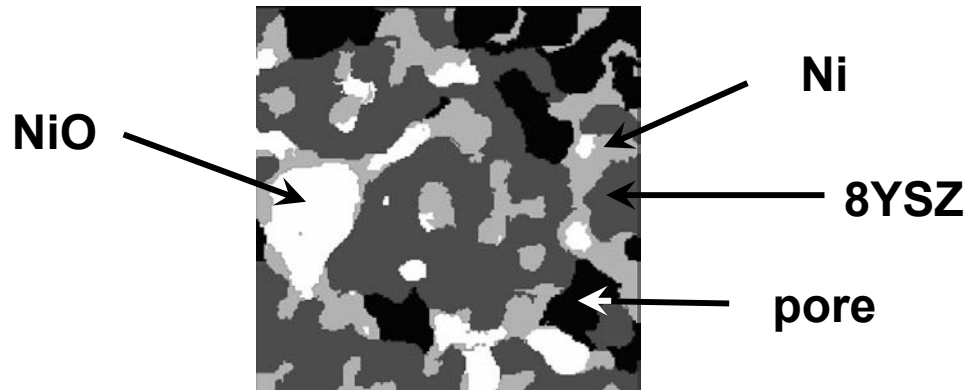


O
white – maximum
Black -minimum

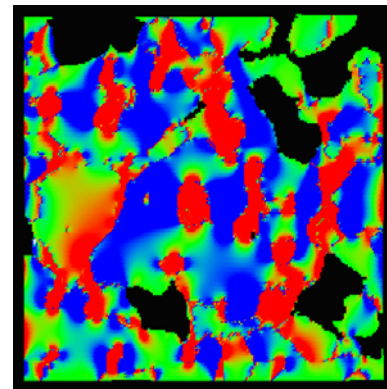


Ni, O, Zr
blue – ZrO
Red – Ni
Yellow – NiO

Compositional Analysis and Micromechanical Stress Modeling



σ_x



σ_y